

MICROCOPY RESOLUTION TEST CHART NATIONAL BUREAU OF STANDARDS-1963-A

THAMES RIVER BASIN

339 AD-A143

LOWER ROSS POND DAM CT. 00175

PHASE 1 INSPECTION REPORT NATIONAL DAM INSPECTION PROGRAM





D

DEPARTMENT OF THE ARMY NEW ENGLAND DIVISION, CORPS OF ENGINEERS WALTHAM, MASS.

AUGUST, 1980

DISTRIBUTION STATEMENT A

Approved for public release; Distribution Unlimited

REPORT DOCUMENTATION PAGE	READ INSTRUCTIONS BEFORE COMPLETING FORM
A .	3. RECIPIENT'S CATALOG NUMBER
CT 00175 A143 3	
4. TITLE (and Subtitle)	INSPECTION REPORT
Lower Ross Pond Dam	INSPECTION REPORT
NATIONAL PROGRAM FOR INSPECTION OF NON-FEDERAL DAMS	6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(s)	8. CONTRACT OR GRANT HUMBER(e)
U.S. ARMY CORPS OF ENGINEERS NEW ENGLAND DIVISION	DACW 37- 80- C- 0013
PERFORMING ORGANIZATION NAME AND ADDRESS CE MA GUIRE INC. 31 Canal Street Providence RI, 02903	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS
11. CONTROLLING OFFICE NAME AND ADDRESS	12. REPORT DATE
DEPT. OF THE ARMY, CORPS OF ENGINEERS NEW ENGLAND DIVISION, NEDED	August 1980
424 TRAPELO ROAD, WALTHAM, MA. 02254	25
14. MONITORING AGENCY NAME & ADDRESS(II dillorent from Centrolling Office)	15. SECURITY CLASS. (of this report)
	UNCLASSIFIED
	18a. DECLASSIFICATION/DOWNGRADING
16. DISTRIBUTION STATEMENT (of this Report)	<u> </u>
APPROVAL FOR PUBLIC RELEASE: DISTRIBUTION UNLIMITED 17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different for	Resert)
18. SUPPLEMENTARY NOTES Cover program reads: Phase I Inspection Report, Nat	ional Dam Inspection Program;
however, the official title of the program is: Nation Non-Federal Dams; use cover date for date of report	t.
DAMS, INSPECTION, DAM SAFETY, Thames River Basin Killingly, Conn.	
Lower Ross Pond Dam 20. ABSTRACT (Centinue on reverse side if necessary and identify by block number)	
N/A	
	ļ

CE MAGUIRE, INC. 31 Canal Street, Providence, Rhode Island 02903

Tel. 401/272-6000

Telex: 92-7533 Cable: CEMI

August 13, 1980

Department of the Army New England Division Corps of Engineers 424 Trapelo Road Waltham, MA 02154

Re: Inspection and Evaluation of Non-Federal Dams FY-80

Connecticut and Rhode Island Contract No. DACW33-80-C-0013

Attn: Mr. P. Gould

Gentlemen:

In accordance with Paragraph 4.a.2.d. of Appendix "A" of the above referenced contract, we hereby, respectfully, submit the following letter report which outlines our reclassification of Lower Ross Pond Dam (CT 00175) to a LOW HAZARD classification.

We trust the information provided is adequate for your staff to agree with our reclassification to LOW HAZARD for this dam. If you have any questions regarding the enclosed data, please contact the undersigned.

It is our understanding that an amendment will be issued by you to our contract, dropping the need for a full study report for both Lower Ross Pond Dam (CT 001752) and Moswamsicut Pond Dam (RI 02002).

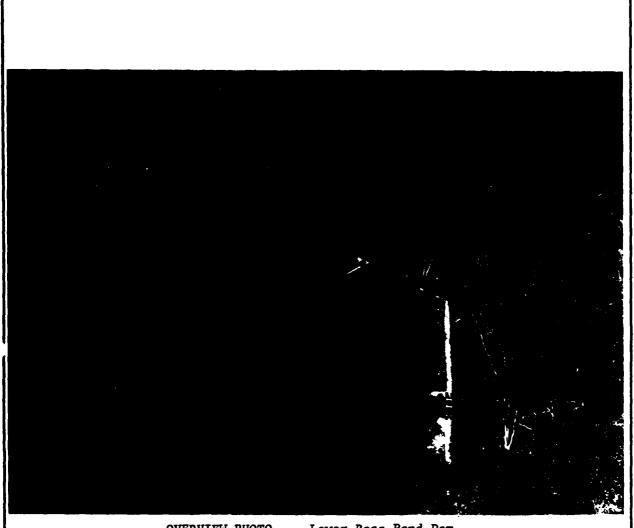
Very truly yours,

CE MAGUIRE INC

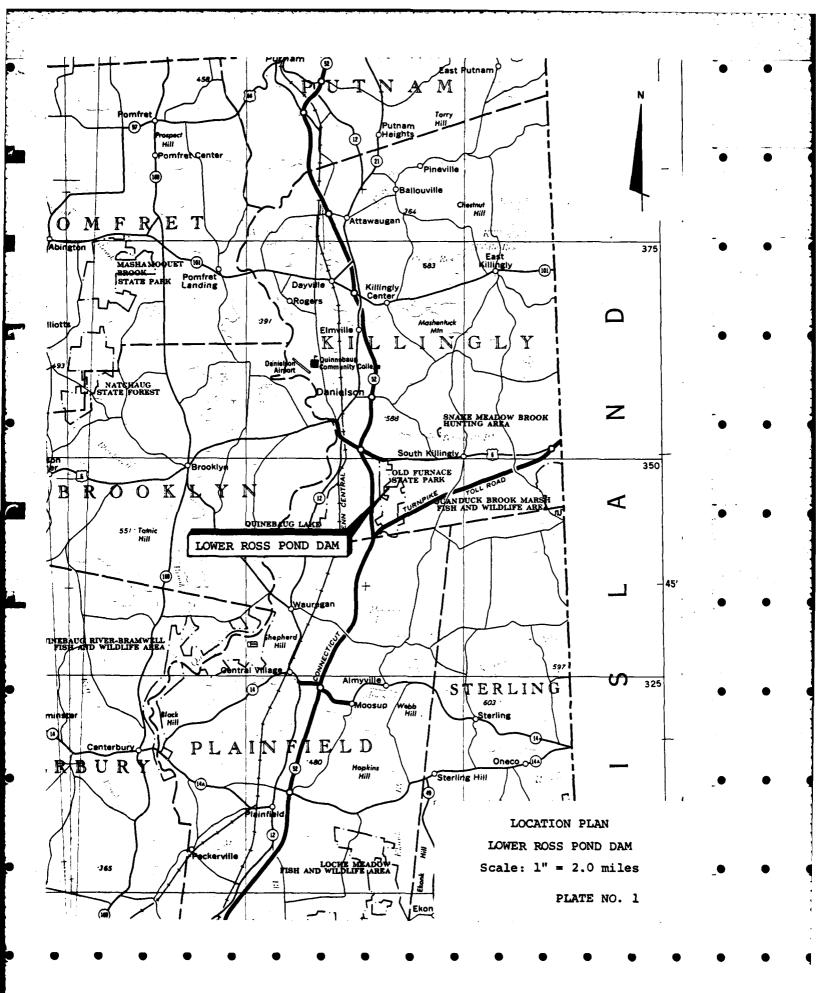
E. A. Reed, P.E.

EAR/jg

Acces	sion For			
NTIS	GRA&I	X	171	
DTIC	TAB			_
Unann	ounced			
Justi	fication		-H. 1	0,7
			-100	-
By				
•	ibution/			
Avai	lability	Codes	-	
	Avail an	d/or		
Dist	Specia	1	ł	
21	1 1		- (
Иh	1 1		- 1	
111	1		- 1	



OVERVIEW PHOTO - Lower Ross Pond Dam



1. Description of the Project

- a. Location: Lower Ross Pond Dam is located in Ross Pond State Park in the Town of Killingly, Windham County, Connecticut, approximately four miles west of the Rhode Island-Connecticut State Boundary along U.S. Route 6. Coordinates of the dam are approximately 41°46.7'N Latitude and 71°51.9'W Longitude. The dam impounds water from a .74-square mile watershed which includes Upper Ross Pond. The terrain is undeveloped, wooded, and moderately sloped.
- b. Description of Dam and Appurtenances: The dam at Lower Ross Pond is approximately 600 feet long, 6 feet high, and is an earth embankment with a downstream stone masonry-concrete capped face. The earth fill section varies in width from 3 to 10 feet along the upstream face and has varying slopes into the pool. The downstream face of the dam is vertical. There are two uncontrolled overflow spillways about 128 feet apart through the dam. The easterly spillway is a masonry and concrete capped weir 12.5 feet long. Short masonry training walls lead into the reservoir pool and channel overflows to the weir section. The downstream channel is Half Hill Brook which meanders through wooded terrain. The westerly spillway weir is 13 feet wide and also has training walls leading into the pond. The easterly spillway crest is approximately 2 feet below the westerly spillway crest. There is no outlet works for the dam.
- c. Size Classification: Ross Pond Dam has an impoundment capacity at the top of the dam (Elev. 335.5 feet NGVD) equal to 40 Ac-Ft. and a height of dam of 7.0 feet. In accordance with the guideline criteria established by the Corps of Engineers, this dam is classified as SMALL in size. The height and impoundment capacity both were the governing criteria in the determination of the SMALL classification.
- d. Hazard Classification: The dam is classified as a LOW HAZARD structure because its failure will not cause: any loss of lives, damage to dwellings, or disruption to public utilities located in the path of the failure flow. The dam failure discharge of 1,386 CFS will have a maximum water depth of approximately 5.0 feet for a distance of 4,000 feet in the impacted area. This small depth of flow will not cause adverse flooding conditions downstream. At a distance of 4,000 feet from the dam, the flooding and depth of flow will diminish to normal acceptable flow conditions and the total outflow of 30 Ac-Ft. will be contained in the available storage downstream.
- e. Ownership: Lower Ross Pond is owned by the State of Connecticut and is managed by the Department of Environmental Protection, Region 4.

f. Operations:

The dam is managed by: Mr. John Olsen, Director

Division of Conservation and Preservation

State of Connecticut

Region 4

and

Mr. John Folsom Unit Manager

Mashamoquet State Park

Pomfret, CT 203/928-6121

- g. Purpose of the Dam: Recreation.
- h. Design and Construction History: The Lower Ross Pond Dam was constructed in the early 1900's. The State of Connecticut purchased both the upper and lower ponds and adjacent lands in June, 1964, and developed Ross Pond State Park. Records of construction are limited; however, it is known that the State in June, 1968, constructed a new gatehouse and drop spillway in the upper pond and regraded the public beach and parking area, also at the Upper Ross Pond. Trees growing adjacent to the lower dam were cut or removed during this contracted work. No record of any other work at the lower dam has been maintained.
- i. Normal Operating Procedures: There are no operating procedures for Lower Ross Pond Dam.

2. Hydraulic/Hydrologic Features

Test Flood Analysis: Recommended guidelines for the Safety Inspection of Dams by the Corps of Engineers were used for selection of the "Test Flood". This Dam is classified under those guidelines as a LOW HAZARD and SMALL size structure. Guidelines indicate that a 50-year to 100-year frequency storm event be used as range of test floods for such classifications. The watershed has a total drainage area of 0.74 square miles. This drainage area is unpopulated, largely wooded, and hilly with rolling terrain. The basin average slope is 0.018 feet/ foot which can be called moderate to flat. The watershed's overall terrain can be classified as rolling. A "test flood" equal to the 100-year frequency event was calculated to equal 400 CSM or 296 CFS for the drainage area. The routed outflow discharge was also developed using the Corps of Engineers criteria for approximate routing and found to be 250 CFS. The upper range (100 year) test flood was selected because of the recreational value of the Pond. Additional design data developed for this investigation is listed in tabular form at the end of this section. The spillway rating curve is illustrated in Appendix D. Flood routings were performed with assumed initial conditions of full a reservoir (ie; spillway crest elevation.)

The spillway capacity is hydraulically inadequate to pass the "test flood" (100-year) and this flow would overtop the by approximately 0.40 feet assuming the overflow length of the dam was equal to 100 feet. The inflow and routed outflow discharge value for this test flood are 296 CFS and 250 CFS, respectively. The maximum outflow capacity of the spillway without overtopping the dam is 142 CFS which is 57 percent of the routed test flood outflow.

b. Dam Failure Analysis: An instantaneous full-depth partial width breach of 40 feet was assumed to have occurred in this dam. This will result in an unsteady flow phenomenon with one flood wave travelling up into the reservoir to feed the other wave travelling downstream into the valley.

With the impounded water level at the top of the dam (Elevation 335.5 feet), the calculated dam failure discharge is 1,386 CFS, and it will produce an approximate water surface elevation of 334.5 feet immediately downstream from the dam. This will raise the water surface an estimated 4.0 feet above the depth of water just prior to failure when the discharge is 142 CFS. The dam failure analysis covered the reach extending from the dam to a distance of 2,000 feet downstream. Normal uniform flow, following Manning's formulae will occur at that point.

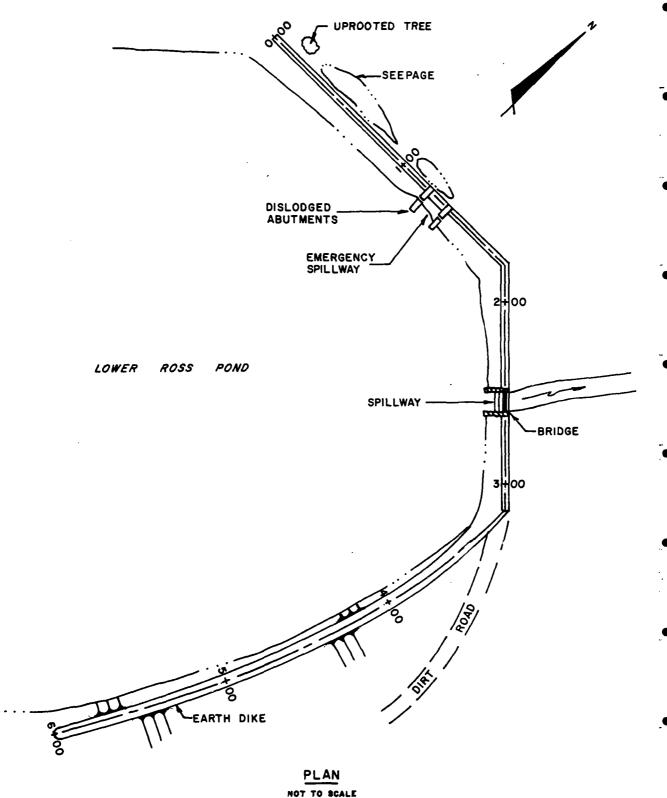
On the assumption that the route I-52 highway embankment structure which is located 2,000 reet downstream from the dam will contain the failure wave, the depth of flow will change from 5.0 feet to 2.0 feet due to the large downstream storage available. The failure discharge will diminish as the reservoir is emptied and depth decreased. River valley storage and frictional losses will tend to reduce the discharge and flow velocities in this reach. Water surface elevations due to the failure of the dam have not been computed because the anticipated depth of flow of 5.0 feet is very small and large storages are available.

LOWER ROSS POND DAM

Inflow, Outflow and Surcharge Data

Table:

FREQUENCY IN YEARS	24-HOUR TOTAL RAINFALL IN INCHES	24-HOUR* EFFECTIVE RAINFALL IN INCHES	MAXIMUM INFLOW IN C.F.S.	MAXIMUM** OUTFLOW IN C.F.S.	HEIGHT	SURCHARGE STORAGE ELEVATION
100	7.0	4.6	296	250	2.9	335.9
= Test Fl	ood					
**Lake as		full at spillway cr	est elevatio	n <u>333.0</u>		
**Lake as	sumed initially dam = 335.	full at spillway cr			methodology	
**Lake as (top of NOTES:	sumed initially dam = 335. Q100; inflow of the Soil Co	full at spillway cr 50)	ted by the a	pproximate m		a
**Lake as (top of NOTES:	sumed initially dam = 335. Q ₁₀₀ ; inflow of the Soil Co Maximum capaci (333.5) is All discharges	full at spillway cr 50) discharges were compu- onservation Service.	ted by the a ithout overt F.S.	pproximate o	dam elevation	
**Lake as (top of NOTES: 1.	Q ₁₀₀ ; inflow of the Soil Co Maximum capaci (333.5) is All discharges upstream stora	full at spillway cr 50 discharges were computed servation Service. ty of the spillway were equal to 142 C. sindicated are dependence reservoirs.	ted by the a ithout overt F.S. dent upon th	pproximate mopping the decontinued	dam elevation	

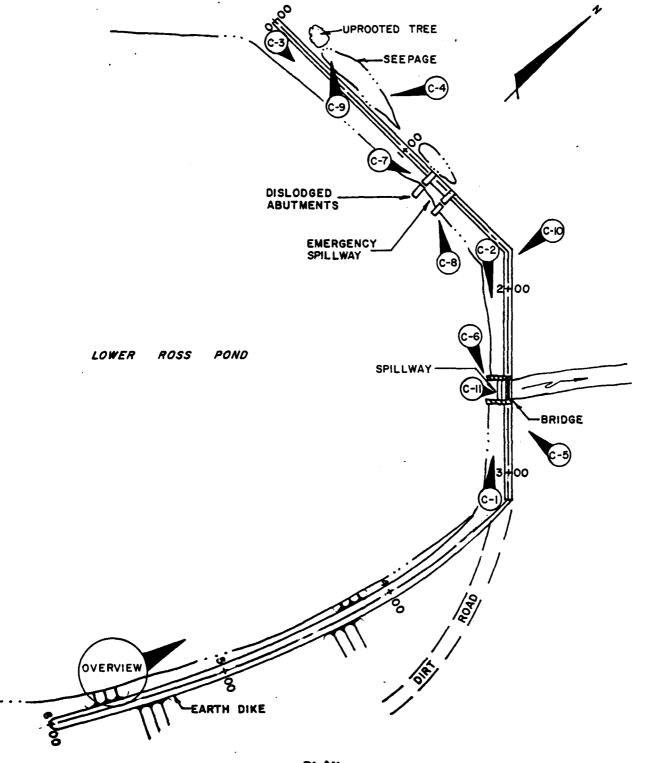


LOWER ROSS POND DAM

PLATE B-I

PLAN OF DAM

APPENDIX



PLAN NOT TO SCALE

LOWER ROSS POND DAM PHOTO INDEX

PLATE C-I



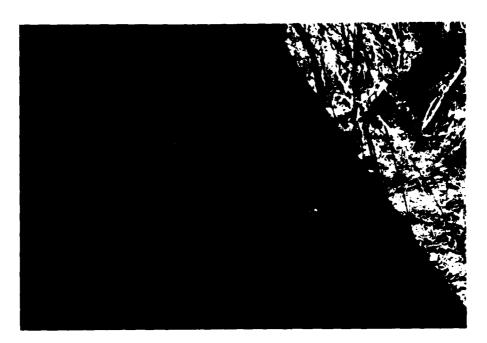
C-1 Crest of Dam looking from right abutment



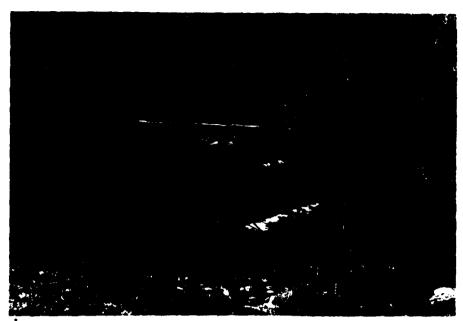
C-2 Crest of Dam looking towards right abutment



C-3 Crest of Dam looking from left abutment



C-4 Seepage at toe of Masonry Dam



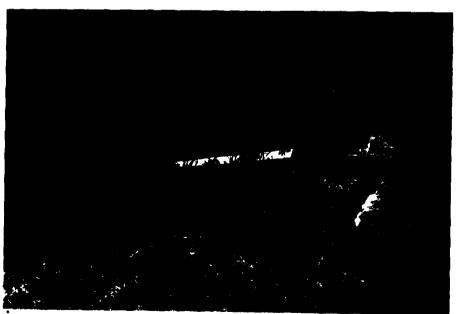
C-5 Right spillway



C-6 Approach to right spillway



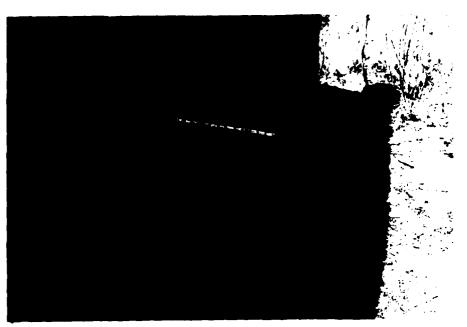
'C-7 Left spillway



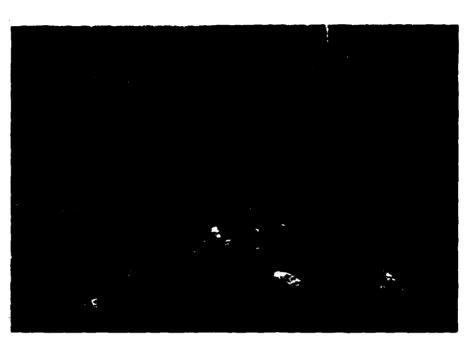
C-8 Left spillway



C-9 Uprooted tree at toe of Masonry Dam



C-10. Tree stump at toe of dam



· C-11 Downstream channel

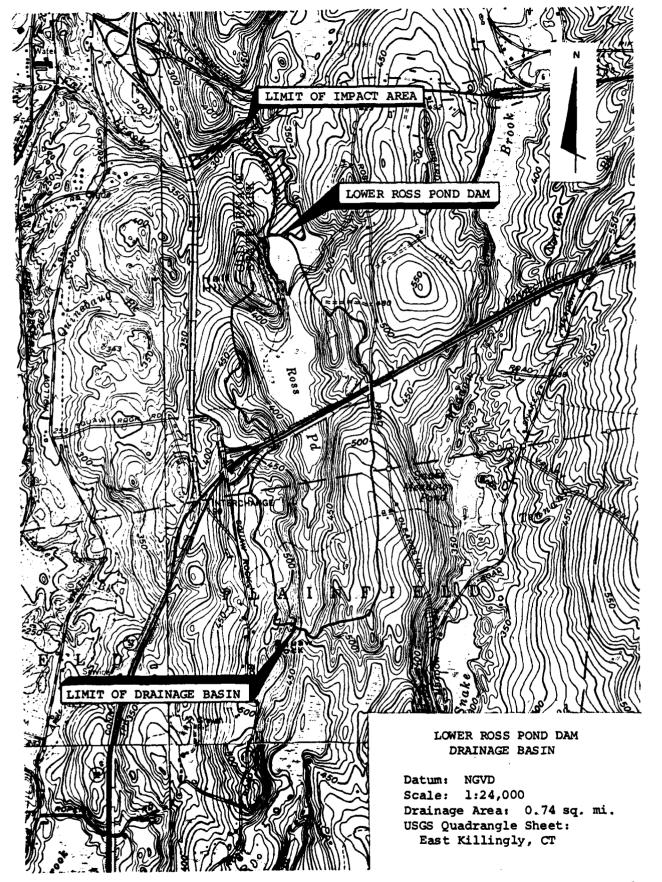


PLATE D-1

A.	Size Classification	LOWER ROSS POND D	<u>AM</u>
Heig	ght of dam =	ft.; hence	SMALL
Sto	rage capacity at top of d	iam (elev.335.50) =	70 AC-FT.; hence SMALL
Ador	pted size classification	SMALL	•
в.	Hazard Potential		
٥.			
	Lower Ross Pon	up Dam is classified as a	LOW hazard
	potential structu	ire because it's failur	e may not cause
	any loss of life	or appreciable propert	y damage. There
		t in the path of the fail	· •
,		e contained within the	
	· · · · · · · · · · · · · · · · · · ·		
	available betwe	en the dam and Route	I-52 without causing
	any appreciable	damage.	
		······································	
c.	Adopted Classification		
HAZ	ARD	SIZE	TEST FLOOD RANGE
	Low	<u>SMALL</u>	50-100 year frequency
Ado	pted Test Flood = 100-	year Frequency Flood PMF	- 400 CSM
			296 cfs
D.	Overtopping Potential		
	Drainage Area	=	
	Spillway crest elevati	on =	333.0 NGVD
	Top of Dam Elevation =		335.5NGVD
	cimum spillway discharge eacity without overtoppin	g of dam =	142 cfs
	est flood" inflow dischar		296 CFS
	st flood" outflow discha	·	250 CFS
	of "test flood" overflow spillway without overtop		57 ° /ø
"te	est flood" outflow disch	arge portion	
whi	ich overflows over the da	m =	108 CF5

% of test flood which overflows over the dam =

Nationaling haximan Probable Discharges - Inflow and Outflow Values but of Inspection: 1704, 1,1980. Howe of Dam Leader Ross Bond Dayn Ideation of Dam Half Hill Brook Trown Killingly, Ct. agr. miles of discharge are as a manage or occupied by fix manage and specifical and a manage or occupied by fix manage and type of Spilluay = 400 CSH 290 CRS Re = Effective Balatil = 4 D.A. = Dealings and type of Spilluay = 12.0 Square Miles Time of Concentration 30 Minutes B. = Midth of Spilluay = 12.0 feet, C = Confficient of Discharge = (309-riction) = 12.0 Top of Dam Elevation = 335.5 Spilluay Creat Elevation 233.0 Top of Dam Elevation 235.5 Spilluay Creat Elevation 233.0 Top of Dam Elevation Spilluay Spilluay Creat Elevation 233.0 Top of Dam Elevation 255.5 Spilluay Creat Elevation 253.0 Top of Dam Elevation 255.5 Spilluay Creat Elevation 253.0 Top of Dam Elevation 255.5 Spilluay Creat Elevation 253.0 Top of Dam Elevation 255.5 Spilluay Creat Elevation 253.0 Top of Dam Elevation 255.5 Spilluay Creat Elevation 255.5 Top of Dam Elevation 255.5 Spilluay Creat Elevation 255.5 Top of Dam Elevation 255.5 Spilluay Creat Elevation 255.5 Top of Dam Elevation 255.5 Spilluay Creat Elevation 255.5 Top of Dam Elevation 255.5 Spilluay Creat Elevation 255.5 Top of Dam Elevation 255.5 Spilluay Creat Elevation 255.5 Top of Dam Elevation 255.5 Spilluay Creat Elevation 255.5 Top of Dam Elevation 255.5 Spilluay Creat Elevation 255.5 Top of Dam Elevation 255.5 Spilluay Creat Elevation 255.5 Top of Dam Elevation 255.5 Spilluay Creat Elevation 255.5 Top of Dam Elevation 255.5 Spilluay Creat Elevation 255.5 Top of Dam Elevation 255.5 Spilluay Creat Elevation 255.5 Top of Dam Elevation 255.5 Spilluay Creat Elevation 255.5 Top of Dam Elevation 255.5 Spilluay Creat Elevation 255.5 Top of Dam Elevation 255.5 Spilluay Creat Elevation

LOWER ROSS POND DAM

COMPUTATIONS FOR SPILLWAY RATING CURVE AND OUTLET RATING CURVE COMPUTATIONS

Spillway wid:	th = 12.0 feet; Spilly	way crest elevation = 333.0 NGVD
Length of dam =	100 feet; Top of	dam elevation = 335.5 NGVD
c = 3.0	for dam and spillway	
i)	SPILLWAY RATING CURVE COMPUTATE	CONS
Elevation (ft.) NGVD	Spillway Discharge (CFS)	Remarks
333.0	. 0	Spillway Crest Elevation
335.5	12.7	
334.0	36.0	
3345	66.0	•
335.O	102.0	
335.5	142.0	Top of Dam Elevation
335.9	177.7	Test Flood Elevation
336.0	293.0	•
336.5	536.0	
ii)	OUTLET RATING CURVE COMPUTATIONS	<u>.</u>
Elevation (ft.) NGVD	Discharge (CFS)	Remarks
	There is no outlet works for Lower Ross Pond Dam	
Size of out		of outlet =sq. ft. er line of outlet =

NAME OF DAM: Lower Ross Pond Dam

ESTIMATING EFFECT OF SURCHARGE STORAGE ON "TEST FLOOD"

- This routing of floods through the reservoir was carried out according to the guidelines established by the Corps of Engineers in Phase 1 Inspection for Dam Safety Investigations issued in March, 1978.
- B. Formulas used are as follows:
 - Q=C,B,H, 3/2 Q=C,B,[h2+F.B.] 3/2+C2B2h2 3/2 For no overtopping: For overtopping: For open channel flow: N/A For orifice flow: N/A where C = coefficient of discharge for spillway; B = length of spillway Cz = coefficient of discharge for dam; Bz = length of dam hi = head over spillway crest (feet); hz = head over dam in feet F.B. = distance between spillway creat and top of dam
 - ii. Surcharge storage in inches = $S = 12 (h_1 + h_2) \frac{S.A.}{D.A.} = 0.26 h$ where S.A. = surface area = 0.0158 $\leq q$. mi. D.A. = drainage area = 0.74 sq. mi.
 - iii. Qoutflow = Qinflow $(1 \frac{S}{Re})$; where Qinflow = 295CFS; $R_e = 4.6$ "
 - overflow Portion)

 Re

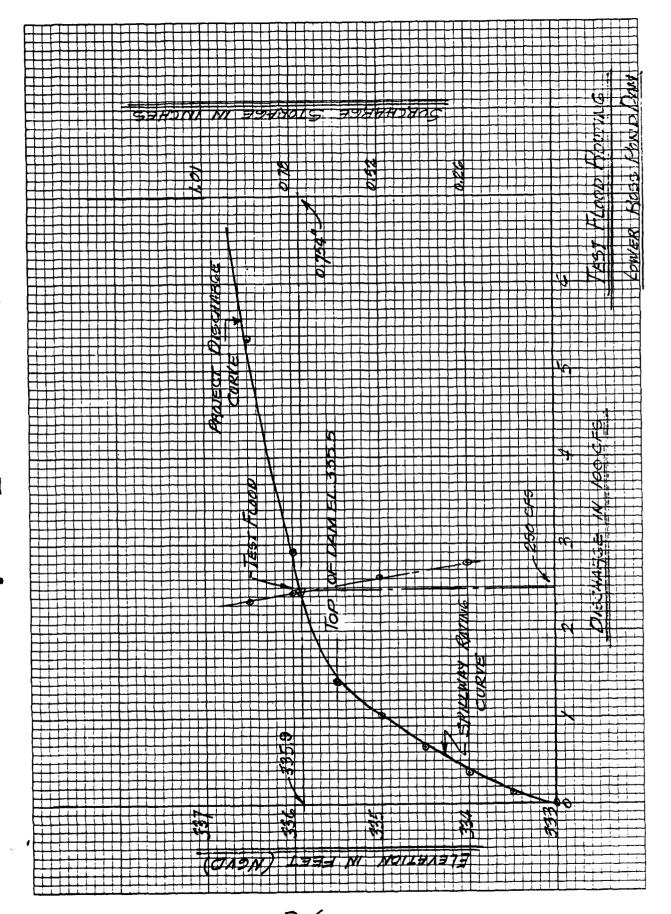
 overflow Portion)

 Re

 iv. Length of dam = 100 feet; Top of Dam elev. = 335.50; c for dam = 3.0

 Length of spillway = 12.0 feet; Spillway crest = 333.0; c for spillway = 3.0
 - Qinflow = 295 C.F.S.

Q in CFS	Elevation	Total Head over crest h ₁ + h ₂ = h	Storage in inches = S	Remarks
278	334.0	1.0	0.26	
270	334.5	1.5	0.39	
262	335.0	2.0	0.52	
253	335.5	2.5	0.65]
245	336.0	3.0	0.78	
237	336.5	3.5	0.91	
250	335.9	2.9	0.754 "	



0-6

"Rule of Thumb Guidance for Estimating Downstream Dam Failure Discharge"

BASIC DATA

Name of dam Lower Ross Pond I	Dam Name of town Killin	aly, Ct.	
Drainage area = 0.74	sq. mi., Top of dam	335.5 feet	NGNT
Spillway type = Broad crested ove	rflow weir Crest of spillway	333.0	GVD
Surface area at crest elevation =	10.10 Acres = 0.0158 sq	.miles	
Reservoir bottom near dam =	328.5 feet NGVD		
Assumed side slopes of embankments _	2:1		
Depth of reservoir at dam site	= y _o =	7.0	_ft.
Mid-height elevation of dam =		332.0	NGVI
Length of dam at crest =		105 feet	
Length of dam at mid-height =		100 feet	
40 of dam length at mid-height = Wb	=	40 feet	

Elevation (NGVD)	I	Estimated Storage in AC-FT		
326.0	0			
333.0	40	Spillway Crest Elevation		
334.0	50	•		
335.a	60			
335 S	70	Top of Dam Elevation		
335. <i>9</i>	75	Test Flood Elevation		

Failure Discharge = 8 WB V9 y 1.5 = 1244

Maximum Spillway Discharge = 142 C.F.S.
Total Failure Discharge = 1386 C.F.S.

NOTE: Dam failure analysis is not carried out due to two reasons a) depth of flow is hardly 5.0 feet b.) 30 AC-FT of storage volume is very small

10002 41 42443 44 445 46 47 48 43 50 51 53 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 6865 70 7172 73 74 75 76 77 78 79 80 C T O O 1 7 5 G 80º IDENTITY NUMBER 97 87 77 36 27 REPORT DATE POPULATION [12] Ş <u>5</u> 20 TATE. D¥ 0A NO Vn RECAUREMENTS CONTROL SYMBOL DAEN-CWE-17 रा बदान बन्ध का प्रमुख्य का का का का कि विदेश कि विद्युक्त कि कि कि कि विद्युक्त कि 1 APRIBO LONGITUDE (West) 7151 FROM DAM (mi) VERIFICATION DATE [61] = FORM APPROVED OMB NO. 49-R0421 [27F] LATHTUDE (North) NAME OF IMPOUNDMENT SCS V. [27E]
PRV/FED [27D]
OWN. [27E] 4 - 46 40NEDNNN <u>0</u> PED. R. ₩ **Q** [14] CORPS ENGR. DIST. [27A] HEIGHT (1) (2) (ACTE (1) (ACTE (1)) (ACTE (1 NEAREST DOWNSTREAM CITY - TOWN - VILLAGE DNAD [18] [27] IMPOUNDING CAPACITIES ROSS 70 OW FE AUREGA [26] 28 NAME INVENTORY OF DAMS IN THE UNITED STATES (PURSUANT TO PUBLIC LAW 92-367) 2 HYDRAULIC HEIGHT (ft) 4 3 ٥ [22] 2 3 14 18 16 17 18 19 20 21 22 23 24 25 26 27 20 20 20 31 32 33 34 35 36 37 38 39 40 8 0 8 0 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 STRUC-TURAL HEIGHT ((1) [24] See reverse side for instructions. RASS 8 9 1011121314151617181920212223242525 272623333333233 PURPOSES [23] L OWER RIVER OR STREAM BROOK [17] [13] 006 S CONGR YEAR COM-PLETED 8 [22] 18 18 20 21 22 HILL PART I 7 9 TSIO E NE PICTON SOR HALF <u>[S</u> TYPE OF DAM COUNTY 8 9 10 11 12/13/14/15 [21] Ξ PREGION © BASIN 0.07 [3] STATE [15] [16] A m DIVISION 2 IDENTIFICATION (Continued) **IDENTIFICATION** STATISTICS LOCATION

E-1

Ξ

ENG FORM 4474

REMARKS

REMARKS

78 79 80 48 49 50|51 52 53 54|55 56|57|58 59|50|61|62|63|64|65|66|67|68|69|70|71|72|73|74|75|76|77|78|79|80| 5 525354 55 5657 38 5960 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 76 Ξ WIDTH (ft) 45 MAINTENANCE LENGTH (fr) [52] [44] WIDTH (ft) [48] [43] LENGTH (ft) [55] NAVIGATION LOCKS [42] WIDTH (11) <u>[</u> LENGTH <u>동</u> WIDTH (ft) 39 [5] 48 49 50 51 LENGTH (ff) [38] [37] REGULATORY AGENCY ЙÖ. ENGINEERING BY PROPOSED (MW) 35 36 37 38 39 40 41 42 43 44 45 [54] [36] 47 POWER CAPACITY INVENTORY OF DAMS IN THE UNITED STATES (PURSUANT TO PUBLIC LAW 92—367) INSTALCED (MW) 35 CONSTRUCTION See reverse side for instructions. [80] 34 NONE 0 9 1011 121314 1516 17 18 19 20 21 22 23 24 22. [53] [33] = SPILLWAY OWNER PART <u>\$</u> 2 1 1011121314151617110 6000U 49 32 WIDTH (ft) 31] 3477 CREST LENGTH (10) 30 6 84 ZYH S/Q @ M MISC. DATA (Continued) MISC DATA STATISTICS

E-2

ENG TOTE 77 4474A

REMARKS

	2		1	_	-	ш
		0		\vdash	ma o Jost de les les les	_
	•				핡	
	11				Ξ	
	1			1	•	
	74 73				-	
					<u>-</u>	
	28 28 74 73		1		-	
	ᅳ	_			=	
	1 2 04 89 89				٤	_
	3				:	
	3				3	
	3				₽	
	99 89 59 49 29 18		1		흙	
	÷				-	_
	1				31	
	3				۷,	
	▣			1	٠,	
	38 3860				3	
					-	
i	-				-	
	13 34 35 36 87				445 46 47 48 99 50 5 125 25 26 26 26 27 28 29 40 9 . 02 16 4 6 2 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	
ļ	8				:	_
	3			'	•	
	103				3	
	35				=	
	ş				Š.	
	49 505 1 52				8.	
	46 47 48				=	
	•				2	
	÷				-	
	•	_		1	•	
	•••	_		i '	•	_
	•				3	
	9				3	
	8				36 37 38 39 40	
	=	_			Ê	_
	Ë			•	E	_
	34 35 34]			_
	5	<u> </u>	l	1	=	—.
	녍	 	ł	1	-	
				!		
	Ê				-	_
	ĕ		l	1	2	
	20 20		l		20 20 20 31 32 39 30 33	
	2				2	_
	4	-	l	İ	2	_
	192 64	-	}		•	
	1	-	1		ट्रा	
	Š		1]	į.	_
	123		l	[27.3	
		-	ļ	1	1202	
	02	-	l	•	-	
			ł	1	=	_
	=		1	!	-	
	3		l	l	•	_
	<u>•</u>	ļ	Į	1	Ę	
	6.	-	ł	1	-	
	13	 	1	ļ		_
	E		1	l	i - i	_
	10]]	亘	
	۴	<u> </u>	ł	l		
	1-	٠	i	┢	ټ.	
			Į.	Ì		
			1	ĺ		
			1	i i		
			1	1		
			1	1		

NED LIGHTS 80 (TEST)

9+84